

Statistical Modeling for the Characteristics of Open Graded Friction Course Asphalt

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Abstract

An open-graded friction course (OGFC) is a special type surface layer of traditional Dense Graded Hot Mix Asphalts (DGHMA) pavement that is increasingly being used around the world due to its various benefits, such as, frictional, safety and environmental, etc. In this research, selective laboratory OGFC properties were statistically modeled depends on mix design inputs for two purposes or aims; mix inputs significant and prediction the OGFC properties according mix inputs. Principally, Indirect Tensile Strength (ITS), water sensitivity (TSR), and permeability (K) were selected from mechanical, durability, and volumetric properties, respectively as an output property; they represent the dependent variables for each model. While, fillers as conventional mineral filler or Ordinary Portland Cement (CMF, or OPC), binder content (BC), and polymer content (SBS) are represented inputs or the independent variables for all models. The generated models offered a vital achievable tool for prediction (e.g., their R^2 are 0.781, 0.821 and 0.820, respectively, for the mentioned model's properties), also it helped to scale the significant of each independent variable (e.g., filler type significantly affect water sensitivity properties, its correlation was 0.752). This study reveals that the statistical modeling is achievable and offers a dynamic tool to describe the characteristics and performance of OGFC mixture in term volumetric, mechanical and durability properties.

Keywords: Asphalt concrete; Open Graded Friction Course; Polymer modified asphalt; Statistical analysis.

1. Introduction.

An open-graded friction course (OGFC) is a special type of asphalt mixtures which characterizes by using open-graded aggregate with high quality properties to ensure a mixture with an elevated connected air voids (AV) content and a course granular structure that improves high stone-on-stone contact. The mixture disintegration and resistance to permanent deformation are provided by stone-on-stone contact of the course-aggregates fraction. Simultaneously, the air void skeleton forms by the coarse aggregates in a compacted specimens is partially occupied by portion of the fine-aggregate [1]. The structure of connected air void in the pavement provides high permeability and reduction in noise, which are directly classified as the main advantages provide by these mixtures when used as surface layer.

Splash and spray reduction help in: reducing wet skidding, reducing hydroplaning risk, and enhancing markings visibility of pavement in wet weather, which are all important advantages of OGFC mixtures [2][3]. Moreover, as compared to traditional Dense Graded Hot Mix Asphalts (DGHMA), the noise reduction effectiveness and riding quality are improved in this type of mixture [4][5]. Furthermore, cleaner runoff has been informed as one of the advantage of OGFC mixtures [6]. finally, smaller concentrations of pollutants related to particulate material and total suspended soils in the runoff gained from OGFC were reported by Several studies as compared to the traditional DGHMA [7][8].

On the other side, some challenges were informed when using OGFC and porous asphalt (PA) mixtures, i.e., mainly are decreased in the structural durability properties of the mixture such as resistance to disintegration and premature voids clogging for the functional durability properties [9][10], relatively high construction cost [9][11], use of limited high-quality materials, like aggregate, reduces structural contribution [12], and winter maintenance issues (e.g., black ice formation) [13].

Durability can identify as the resistance of the mixture to subsequent failures and distresses within the lifespan of the pavement layers under different loading and weather conditions. Raveling was reported as the most important distresses in OGFC in addition to the common distresses such as rutting (due to studded tires), reflective cracking, and delamination (which is principally caused by construction problems) [14].

Numerous causes for raveling development like hardening due to high rate of oxidation as a result of elevated air voids [15][16], deficiency in compaction [17], insufficient temperature during construction [18], and volumetric properties problems (e.g., incorrect calculation of binder content and/or air void content or lack of control of these properties during construction) [19][20]. Numerous numerical and experimental models have been recommended to enhance understanding and predicting of raveling occurrence. The conclusion of these efforts is that raveling is mostly influenced by the total air voids content in the mixture and its binder content [21], however different parameters like the number of cold days at the project site and the coarse aggregate fraction also showed to influence both the appearance and magnitude of this distress [22] [23].

However, the main purpose of this study is to develop statistical models for predicting some volumetric, mechanical, and durability properties according to the variation in some main mix parameters. This prediction process could facilitate the understanding of the role of these parameters in general mix characteristics. Therefore, this paper will discuss the analysis process for built and validate the prospective models.

2. Research materials and methodology.

2.1 Raw material.

Limestone aggregates were supplied from local quarries, which is located to the west of Karbala. The physical properties of the aggregates present in Table (1). They were crushed limestone aggregate with a degree of crushing exceed 90%. The ASTM D7064 proposed gradation range for OGFC and the middle range of each size was selected to prepare the mixes in this research work. Figure (1) displays the particle size distribution, which falls within the suggested lower and upper limits in ASTM D7064 gradation.

Table 1 Used aggregate physical properties.

Measured properties	Standard (ASTM)	Value
Coarse Aggregate Bulk Specific Gravity (gr/cm ³)	C127[24]	2.591
Abrasion Value of Los Angeles (%)	C131[25]	21.5
Fine Aggregate Bulk Specific Gravity (gr/cm ³)	C127[24]	2.322
Coarse Aggregate Water Absorption (%)	C127[24]	2.22
Fine Aggregate Water Absorption (%)	C127[24]	2.41
One Side Fractured Particles %	D5821[26]	97.0
Two Sides Fractured Particles %	D5821[26]	95.0

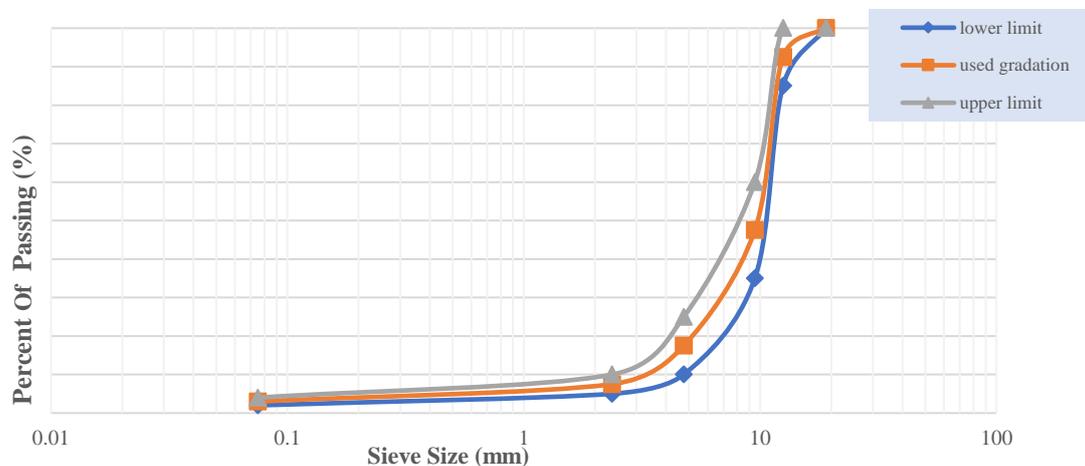


Figure 1 Particle size distribution of recommended range and used middle gradation[32] have a direct effect on mechanical properties for the GRC. Two types of fillers were used in this research; namely, Ordinary Portland Cement (OPC), and Conventional Mineral Filler (CMF). Table (2) identifies physical and chemical properties for used fillers.

Table 2 The physical and chemical properties of OPC and CMF fillers.

Physical		
Property	Filler Type	
	CMF	OPC
surface Area (m²/kg)	223	345
Density (gm/cm³)	2.650	2.981
Chemical		
SiO₂	81.89	25.410
Al₂O₃	3.78	2.324
Fe₂O₃	1.92	1.125
CaO	7.37	65.148
MgO	3.45	1.326
K₂O	0.73	0.760
Na₂O	0.19	1.714

The used bitumen was nominated with penetration grade (40–50), it was supplied from Al-Neasseria in the South of Iraq. The selected neat bitumen cement meet the specification in ASTM D946 [27]. Also, it was modified with SBS polymer called Kraton D1192 ESM. the properties of the neat and modified bitumen are presented in Table (3). while Table (4) illustrates the SBS polymer properties. The process of polymer-modified asphalts is not common procedure in Iraq. Thus, the SBS polymer and asphalt cement were prepared in the university of Kerbala laboratory.

Table 3 Properties of the neat and modified bitumen.

Properties	Standard (ASTM)	0SBS	2SBS	4SBS	6SBS
Penetration at 25 °C (0.1 mm)	D5-73[28]	41.47	2.5	2.1	1.87
(Ring and ball) Softening point °C	C36-76	47.5	51	56	60.5
Ductility at 25 °C (cm)	D113-79	>100 cm	>100 cm	80 cm	76 cm
P.I.	[29]	-2.23	-2.30	-1.56	-0.79
AFTER thin-film oven test (TFOT)					
Penetration at 25 °C (0.1 mm)	D5-73[30]	2.90	2.38	2.00	1.8
(Ring and ball) Softening point °C	C36-76	50.5	53	66.5	68
Mass Change, %	D1754/D1754M – 09 (Reapproved 2014) Standard[31]	0.03	0.01	0.00	0.00

Table 4 Kraton D1192 ESM polymer properties.

Property	Test Method	Unit	Tested Value
Specific Gravity	SO 2781	-----	0.94
Melt Flow Rate, 200°C/5kg	ISO 1133	g/10min.	<1
Bulk Density	ASTM D 1895 method B	kg/dm ³	0.4
Hardness, Shore A (15 sec) a	ASTM D 2240	Hardness, Shore A (15 sec)	70
Apparent Molecular Mass of Triblock	KM 01	kg/mol.	150
Ash (ETM)	BAM 908	%w	5.0
Polystyrene Content	KM 03	%m	30.5
Triblock Content	KM 01	%	90
Vinyl Content	KM 03	%	35
Volatile Matter	KM 04	%m	0.3
Total Extractables	KM 05	%m	1.0
Antioxidant Content	KM 08	%m	0.16
Ash (ES, ET)	ISO 247	%m	0.25
Ash (ESM)	ISO 247	%m	3.75

2.2 Mixture design and analysis.

Two OGFC mix types were included in this study i.e., traditional and modified mixes. The traditional mixture contained neat binder grade 40-50 type, virgin Coarse and fine aggregates, with CMF, OPC filler types. The selected of aggregate gradation was based on ASTM D7064[32] as cleared previously in Figure (1). Therefore, to determinate the characteristics of this mix, six different asphalt contents ranging between 5%-7.5% in increments of 0.5 % is introduced. The bitumen contents 6%-7% were found, corresponding to best durability and volumetric properties that satisfy limitations of ASTM D7064 criteria; i.e., cantabro, air-voids, and draindown test results.

In this study, only three parameters were selected from mechanical, volumetric and durability properties to develop statistical models. However, the volumetric properties of OGFC mixes with two-filler types and four polymer content and six-asphalt content were characteristic. Main indexes like bulk density, air void, effective Porosity, VFB, and VMA, permeability, draindown, were determined and analyzed according to ASTM D7064[32], while the permeability was selected to represent the volumetric properties. The mechanical properties of OGFC were characterized by many tests; i.e., Indirect Tensile strength, Marshall Stability and flow, wheel truck test, skid resistance with the same mix design inputs. While, Indirect tensile strength (IDT) test according to AASHTO T283[33] was selected as an important test to represent the mechanical properties of the OGFC. Similarly, the durability properties were evaluated by tensile strength ratio (TSR) test according to AASHTO T283[33]. It is worth mentioned that in details models for each volumetric, mechanical, and durability properties will present in future publication.

2.3 Collected Data.

The input data (results) of permeability (as an average of four samples results), ITS (as an average of three samples results), and TSR (as an average of three set results) each set comprised two conditioned and unconditioned samples). A total of 639 test results were collected and analyzed in (SPSS) software to extract the averaged results which used to build the model, the input averaged data are as presented in Table (5) below:

Table 4 Results Matrix.

<i>Mix no.</i>	<i>Mix design Input parameters</i>			<i>Mix characteristic indexes</i>		
	<i>Filler type</i>	<i>SBS, %</i>	<i>BC, %</i>	<i>Permeability (K), cm/sec</i>	<i>ITS, KPa</i>	<i>TSR, %</i>
<i>P5MO-0</i>	OPC	0	5	186.1	282.59	93.22

	OPC	0	5	188.29	-----	-----
P5.5MO-0	OPC	0	5.5	142.87	586.39	94.34
	OPC	0	5.5	174.11	-----	-----
P6MO-0	OPC	0	6	169.64	609.28	95.23
	OPC	0	6	137.81	-----	-----
	OPC	0	6	139.80	-----	-----
	OPC	0	6	134.22	-----	-----
P6.5MC-0	CMF	0	6.5	-----	699.77	41.37
	CMF	0	6.5	-----	686.26	43.36
	CMF	0	6.5	-----	693.02	43.69
	CMF	0	6.5	-----	----	41.82
	CMF	0	6.5	-----	----	44.9
P6.5MO-0	OPC	0	6.5	75.98	569.88	65.55
	OPC	0	6.5	142.34	538.24	95.8
	OPC	0	6.5	99.51	569.88	83.1
	OPC	0	6.5	124.95	554.06	63.65
	OPC	0	6.5	110.69	----	62.74
	OPC	0	6.5	110.69	----	95.8
	OPC	0	6.5	110.69	----	----
P7MO-0	OPC	0	7	103.05	537.19	94.12
	OPC	0	7	103.05	----	----
	OPC	0	7	77.21	----	----
	OPC	0	7	83.57	----	----
	OPC	0	7	103.05	----	----
	OPC	0	7	103.04	----	----
	OPC	0	7	103.05	----	----
P7.5MO-0	OPC	0	7.5	106.72	290.71	93.01
	OPC	0	7.5	100.17	----	----
	OPC	0	7.5	103.44	----	----
P6MO-2	OPC	2	6	213.6	----	----
	OPC	2	6	251.75	----	----
	OPC	2	6	180.6	----	----
P6.5MO-2	OPC	2	6.5	188.69	823.99	95.1
	OPC	2	6.5	209.16	709.54	89
	OPC	2	6.5	232.79	759.49	94.99
	OPC	2	6.5	174.77	701.88	87.5
	OPC	2	6.5	200.58	734.52	95.6
P6.5MC-2	CMF	2	6.5	202.72	679.66	76.6
	CMF	2	6.5	219.59	627.71	76.25
	CMF	2	6.5	211.15	680.85	74
	CMF	2	6.5	----	768.25	73.88

	CMF	2	6.5	----	654.28	74.12
<i>P7MO-2</i>	OPC	2	7	162.52	----	----
	OPC	2	7	186.48	----	----
	OPC	2	7	168.51	----	----
	OPC	2	7	184.95	----	----
<i>P6.5MO-4</i>	OPC	4	6.5	152.88	715.03	93.1
	OPC	4	6.5	158.74	707.52	88.6
	OPC	4	6.5	153.77	627.02	93.05
	OPC	4	6.5	136.45	677.62	91.11
	OPC	4	6.5	150.46	----	----
<i>P6.5MC-4</i>	CMF	4	6.5	296.8	627.36	68.06
	CMF	4	6.5	247.51	657.64	67.11
	CMF	4	6.5	223.17	783.25	66.46
	CMF	4	6.5	282.04	719.61	67.21
	CMF	4	6.5	262.38	720.45	----
<i>P6MO-4</i>	OPC	4	6	182.73	610.3	----
	OPC	4	6	184.01	667.27	----
	OPC	4	6	171.42	----	----
	OPC	4	6	168.83	----	----
	OPC	4	6	206.64	----	----
<i>P6.5MC-6</i>	CMF	6	6.5	251.96	819.94	50.91
	CMF	6	6.5	218.28	----	50.91
	CMF	6	6.5	235.12	----	43.4
<i>P6.5MO-6</i>	OPC	6	6.5	145.46	779.96	76.8
	OPC	6	6.5	141.85	803.72	78.3
	OPC	6	6.5	143.97	791.84	77.5
	OPC	6	6.5	130.62	----	----
<i>P7MO-4</i>	OPC	4	7	162.15	----	----
	OPC	4	7	167.85	----	----
	OPC	4	7	129.99	----	----
	OPC	4	7	115.65	----	----
<i>P6MO-6</i>	OPC	6	6	178.25	----	----
	OPC	6	6	205	----	----
	OPC	6	6	225.82	----	----
	OPC	6	6	195.55	----	----
	OPC	6	6	173.11	----	----
<i>P7MO-6</i>	OPC	6	7	105.18	----	----
	OPC	6	7	107.58	----	----

3. Statistical analysis model.

3.1 Model preparation.

Model preparation from the outcomes that obtained in the experimental work is an essential in this research. Empirical modeling was achieved using analysis tools of SPSS software. The variables involved in the empirical modeling were filler types, binder content, and percent of SBS. The collected averaged results are 72,40, and 37 for each test of permeability, tensile strength ratio, and indirect tensile strength, respectively, consequently, a total of 639 test result were collected and analysis. The results were divided randomly into 49, 30, 28 result to generate the model and the other 23, 10, 9 for each test of permeability, TSR, and ITS, respectively, were used to validate the model. The first step to model preparations is to the correlation between the variables using SPSS Pearson's correlation. Many combinations of variables were used starting from only constant to quadratic form of the variables with the incorporation of multiple terms of the various variables discussed above.

To achieve the obligations for the built models, program testing needs to determine dependent and independent variables of the developed models. The variables and the code adopted for calculation are presented in Table (6).

Table 5 Dependent and independent variables considered in regression analysis.

<i>Dependent variable</i>			
<i>Abbrev.</i>	<i>Descrip.</i>	<i>Unit</i>	<i>Coded values</i>
<i>ITS</i>	<i>Indirect tensile strength</i>	<i>KPa</i>	
<i>K</i>	<i>permeability</i>	<i>mm</i>	
<i>TSR</i>	<i>Water sensitivity</i>	<i>%</i>	
<i>Independent variable</i>			
<i>FT</i>	<i>Filler type</i>	<i>CMF</i>	<i>15</i>
		<i>OPC</i>	<i>20</i>
<i>SBS</i>	<i>Polymer content</i>	<i>%</i>	
<i>BC</i>	<i>Binder content</i>	<i>%</i>	

4. Result and Discussion for The Prediction Models.

SPSS software was used to build and analysis the models. For the simplification the linear models were tried first, unfortunately, the trials that made for linear models were unsuccessful to represent the observations. However, it was found that all prediction models were nonlinear, as will see hereafter.

4.1 Building the permeability model.

As mentioned previously the Permeability was selected to build a model from many volumetric parameters. This selection is established on the believe that it is the most important character. Modeling permeability to filler type, binder content, and polymer content was conducted. Many models were tried (linear, multiple and nonlinear models). It was observed that all linear models were failed to estimate accurate predicted values of permeability. Tables (7) demonstrates samples of the tried models, whereas low values of (R^2) are the predominant for both regression and model validation. It is worth mentioned that other testing parameters than R^2 were conducted to test the validity of the models, but the values of R^2 are only presented for simplification and prevent dilatation.

On the other hand, after many trials a nonlinear model was determined with reasonable accuracy. The analysis results of adopted nonlinear model is shown in Tables (8), (9), and (10). The model's analysis consists of the analysis of goodness fitting and variance for observed and predicted result. The model adequacy is illustrated in figure (2). The following can be recognized from the analysis process:

1. Table (8) explains the bivariate Pearson Correlation between variables. The same table shows that the independent variables have very low to absent of correlation between each other, which is good for the accuracy of the model.
2. Table (8) demonstrates that the filler type has the most significant correlation to permeability, then binder content and lastly polymer content. Although, binder content is believed to be the most important, but we have to remember that the used ranges of building the model is limited.
3. Table (10) states that the MSE is low, which is good for the significant of the model.

4. Table (9) shows the parameter of the developed model and its limitation with Confidence Interval of 95%.
5. Table (10) discloses that the sum of regression is higher than sum of residue which is sustained the significant of the model. While, from the same table, the high value of the R-Square (0.781) indicates an acceptable prediction.
6. Figure (2) indicates that acceptable scatter can be recognized between predicted and observed K values, furthermore, almost all values within the significant level boundaries.

Table 6 Trial Equations to Predict The Value of Permeability.

Types of equations	models	R ²
linear	$k = 717.7 + 5.71 * sbs - 16.3 * ft - 39.4 * bc$	0.621
linear	$k = 507.3 - 17.8 * ft$	0.401
cubic	$k = 507.3 - 17.7 * ft$	0.401
compound	$k = 1042.2 + 0.907 * ft$	0.311
logarithmic	$k = 24223.4 - 1.7 * \ln ft$	0.311
nonlinear	$k = 147.8 + 0.056 * sbs * ft * bc$	0.095
nonlinear	$k = 145.88 + 2.6 * \left(\frac{sbs * ft}{bc}\right)$	0.12
nonlinear	$k = 306.8 + 0.486 * sbs^2 - 0.003 * ft^3 * bc$	0.553
nonlinear	$K = 435.6 - 0.908 * sbs * bc - 2.29 * ft * bc$	0.612

Table 7 Correlation Between Permeability and Variables.

Correlations					
		SBS	FT	BC	K
SBS	Pearson Correlation	1	-.205	.038	.276*
	Sig. (2-tailed)		.077	.744	.017
	No.	75	75	75	75
FT	Pearson Correlation	-.205	1	-.017	-.631**
	Sig. (2-tailed)	.077		.886	.000
	No.	75	75	75	75
BC	Pearson Correlation	.038	-.017	1	-.396**
	Sig. (2-tailed)	.744	.886		.000
	No.	75	75	75	75
K	Pearson Correlation	.276*	-.631**	-.396**	1
	Sig. (2-tailed)	.017	.000	.000	
	No.	75	75	75	75

*. Correlation is significant at the 0.05 level (2-tailed).
 **. Correlation is significant at the 0.01 level (2-tailed).

Table 8 Nonlinear permeability modeling

Developed model	$K = c1 + c2 * BC + c3 * BC^2 + c4 * SBS - c5 * SBS^2 + c6 * SBS^3 - c7 * FT$			
Parameter Estim.				
Parameter	Estim.	Std. Err.	95% Confidence Interval	
			Lower Bound.	Upper Bound.
c1	1110.146	345.026	421.658	1798.634
c2	169.623	107.030	-43.951	383.198
c3	9.783	8.393	-6.966	26.531
c5	22.059	5.256	11.572	32.547
c6	1.836	.571	.697	2.975
c7	15.276	1.737	11.810	18.742
c4	71.171	12.083	47.059	95.283

Table 9 ANOVA for permeability modeling

<i>ANOVAa</i>			
<i>Source</i>	<i>Sum of Squares</i>	<i>df</i>	<i>Mean Squares</i>
<i>Regression</i>	2149248.823	7	307035.546
<i>Residual</i>	43006.629	68	632.450
<i>Uncorrected Total</i>	2192255.452	75	
<i>Corrected Total</i>	195946.010	74	

Dep. variable: K

a. R squared = 1 - (Residual Sum of Squares) / (Corrected Sum of Squares) = .781.

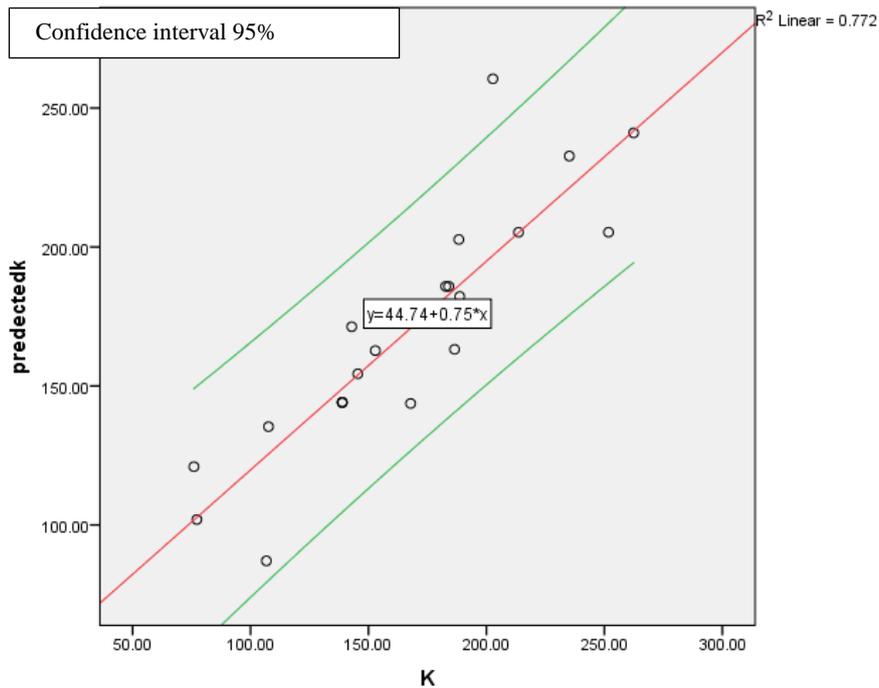


Figure 2 comparisons between the experimental and predicted values of permeability.

4.2 Building the Tensile strength ratio modal.

As mentioned previously the TSR was selected to build a model from many durability parameters. This selection is established on the believe that it is the most important durability character. Modeling TSR to filler type, binder content, and polymer content was conducted. Many models were tried (linear, multiple and nonlinear models). It was observed that all linear models were failed to estimate accurate predicted values of TSR. Tables (11) demonstrates samples of the tried models, whereas low values of (R^2) are the predominant for both regression and model validation. It is worth mentioned that other testing parameters than R^2 were used to test the validity of the models, but the values of R^2 are only presented for simplification and prevent dilatation.

On the other hand, after many trials a nonlinear model was determined with reasonable accuracy. The analysis results of adopted nonlinear model are shown in Tables (12), (13), and (14). The model’s analysis consists of the analysis of goodness fitting and variance for observed and predicted result. Figure (3) demonstrates the adequacy of model. The following can be recognized from the analysis process:

1. Table (12) explains the bivariate Pearson Correlation between variables. The same table shows that the independent variables have very low to absent of correlation between each other, which is good for the accuracy of the model.
2. Table (12) demonstrates that the filler type has the most significant correlation to TSR, then polymer content and lastly binder content.

3. Table (14) states that the MSE is low, which is good for the significant of the model.
4. Table (13) shows the parameter of the developed model and its limitation with Confidence Interval of 95%.
5. Table (14) discloses that the sum of regression is higher than sum of residue which is sustained the significant of the model. While, from the same table, the high value of the R-Square (0.821) indicates a good prediction, thus from this value a conclusion can draw that the developed model for Tensile strength ratio is acceptable.
6. Figure (3) indicates that acceptable scatter can be recognized between predicted and observed operability values, furthermore, almost all value within the significant level boundaries.

Table 10 Trial Equations to Predict The Value of Tensile strength ratio.

<i>Types of equations</i>	<i>Models</i>	<i>R²</i>
Linear	$TSR = -7.9 - 0.024 * sbs - 2.33 * bc + 5.52 * ft$	0.569
Linear	$TSR = 24.5 + 5.57 * ft$	0.566
Cubic	$TSR = 23.25 + 0.159 * ft^2$	0.566
Compound	$TSR = 16.967 + 1.09 * ft$	0.536
Logarithmic	$TSR = 1.25 + 1.41 * \ln ft$	0.536
Nonlinear	$TSR = 115.3 + 0.002 * sbs * ft - 6.339 * bc$	0.014
Nonlinear	$TSR = 33.6 - 1.6 * 10^{-11} * ft^2 * sbs^5 * bc + 0.008 * bc^3 * ft$	0.245
Nonlinear	$TSR = 8.176 - 0.003 * ft * sbs + 0.733 * bc * ft$	0.451
Nonlinear	$TSR = -7.9 - 0.024 * sbs - 2.33 * bc + 5.52 * ft$	0.569

Table 11 correlation between TSR and variables.

<i>Correlations</i>					
		<i>TSR</i>	<i>sbs</i>	<i>BC</i>	<i>FT</i>
<i>TSR</i>	<i>Pearson Correlation</i>	1	-.128	-.116	.752**
	<i>Sig. (2-tailed)</i>		.430	.476	.000
	<i>No.</i>	40	40	40	40
<i>sbs</i>	<i>Pearson Correlation</i>	-.128	1	.097	-.135
	<i>Sig. (2-tailed)</i>	.430		.550	.407
	<i>No.</i>	40	40	40	40
<i>BC</i>	<i>Pearson Correlation</i>	-.116	.097	1	-.094
	<i>Sig. (2-tailed)</i>	.476	.550		.564
	<i>No.</i>	40	40	40	40
<i>FT</i>	<i>Pearson Correlation</i>	.752**	-.135	-.094	1
	<i>Sig. (2-tailed)</i>	.000	.407	.564	
	<i>No.</i>	40	40	40	40

**. Correlation is significant at the 0.01 level (2-tailed).

Table 12 Nonlinear TSR modeling

<i>Developed model</i>	$TSR = c1 + c2 * sbs - c3 * sbs^2 + c4 * sbs^3 - c5 * bc + c6 * bc^3 + c7 * FT$				
<i>Parameter Estim.</i>					
<i>Parameter</i>	<i>Estim.</i>	<i>Std. Err.</i>	<i>95% Confidence Interval</i>		
			<i>Lower Bound.</i>	<i>Upper Bound.</i>	
<i>c1</i>	262.594	114.196	30.260	494.927	
<i>c2</i>	5.940	1.442	3.007	8.873	
<i>c3</i>	.158	.048	.060	.255	
<i>c4</i>	.001	.000	.000	.002	
<i>c5</i>	80.307	27.208	24.952	135.662	
<i>c6</i>	.655	.232	.183	1.126	
<i>c7</i>	5.607	.567	4.454	6.761	

Table 13 ANOVA for TSR modeling

ANOVAa			
Source	Sum of Squares	df	Mean Squares
Regression	236488.154	7	33784.022
Residual	2393.275	33	72.523
Uncorrected Total	238881.429	40	
Corrected Total	13398.602	39	
Dep. variable: TSR			
a. R squared = 1 - (Residual Sum of Squares) / (Corrected Sum of Squares) = .821.			

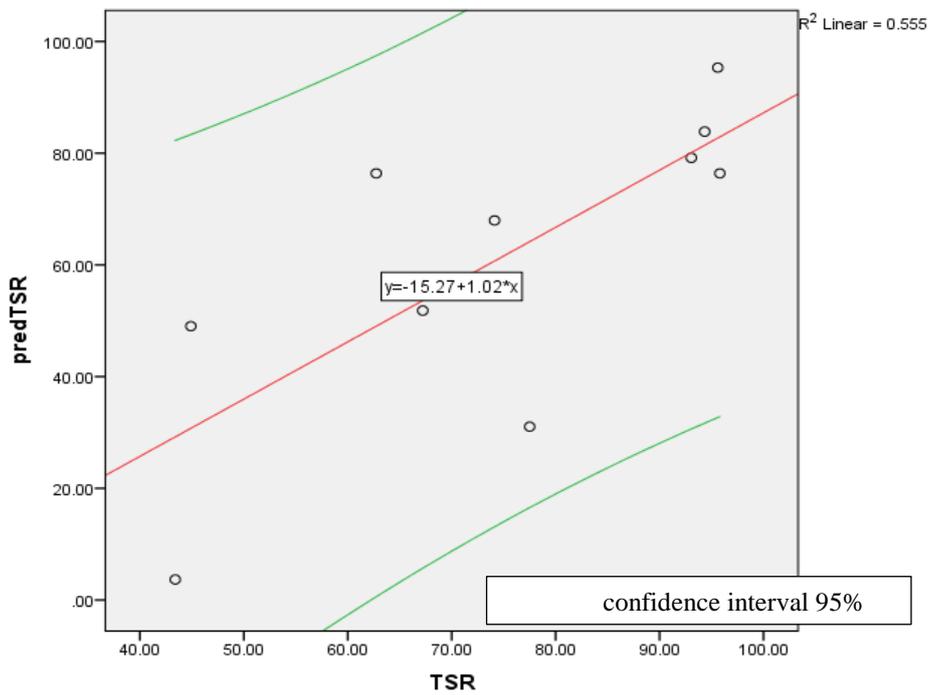


Figure 3 comparisons between the experimental and predicted values of TSR.

4.3 Building the Indirect tensile strength model.

As mentioned previously the ITS was selected to build a model from many Mechanical parameters. This selection is established on the believe that it is the most important mechanical character. Modeling ITS to filler type, binder content, and polymer content was conducted. Many models were tried (linear, multiple and nonlinear models). It was observed that all linear models were failed to estimate accurate predicted values of ITS. Tables (15) demonstrated samples of the tried models, whereas low values of (R^2) are the predominant for both regression and model validation. It is worth mentioned that other testing parameters than R^2 were used to test the validity of the models, but the values of R^2 are only presented for simplification and prevent dilatation.

On the other hand, after many trials a nonlinear model was determined with reasonable accuracy. The analysis results of adopted nonlinear model are shown in Tables (16), (17), and (18). The model's analysis consists of the analysis of goodness fitting and variance for observed and predicted results. Figure (4) demonstrates the adequacy of model. The following can be recognized from the analysis process:

1. Table (16) explained the bivariate Pearson Correlation between variables. The same table shows that the independent variables have low to absent of correlation between each other, which is good for the accuracy of the model.

2. Table (16) demonstrates that the polymer content has the most significant correlation to ITS, then filler type and lastly binder content.
3. Table (18) states that the MSE is low, which is good for the significant of the model.
4. Table (17) shows the parameter of the developed model and its limitation with Confidence Interval of 95%.
5. Table (18) discloses that the sum of regression is higher than sum of residue which is sustained the significant of the model. While, from the same table, the high value of the R-Square (0.820) indicates a perfect prediction, thus from this value a conclusion can draw that the developed model for ITS is acceptable.
6. Figure (4) indicates that acceptable scatter can recognize between predicted and observed operability values, furthermore, almost all value within the significant level boundaries.

Table 14 Trial Equations to Predict The Value of Indirect tensile strength.

Types of equations	Models	R ²
Linear	$ITS = 621.6 + 3.81 * sbs + 22.6 * bc - 11.57 * ft$	0.367
Linear	$ITS = 555.02 + 3.93 * sbs$	0.303
Cubic	$ITS = 145.8 + 55.8 * sbs - 1.6 * sbs^2 + 0.16 * sbs^3$	0.489
Compound	$\ln ITS = 539.3 + 1.007 * sbs$	0.244
Logarithmic	$\ln ITS = 358.8 + 0 + 19 * \ln sbs$	0.297
Nonlinear	$ITS = 568 + 0.029 * bc * sbs * ft$	0.29
Nonlinear	$ITS = 713.2 + 3.95 * sbs - 1.357 * bc * ft$	0.34
Nonlinear	$ITS = 621.6 + 3.81 * sbs + 22.6 * bc - 11.6 * ft$	0.367
Nonlinear	$ITS = 1092.18 - 7.59 * sbs - 1.3 * bc - 28.57 * ft + 0.095 * sbs * bc * ft$	0.405

Table 15 correlation between ITS and variables.

Correlations					
		SBS	BC	FT	ITS
sbs	Pearson Correlation	1	.117	-.039	.551**
	Sig. (2-tailed)		.491	.818	.000
	No.	37	37	37	37
bc	Pearson Correlation	.117	1	-.089	.152
	Sig. (2-tailed)	.491		.601	.371
	No.	37	37	37	37
ft	Pearson Correlation	-.039	-.089	1	-.264
	Sig. (2-tailed)	.818	.601		.114
	No.	37	37	37	37
ITS	Pearson Correlation	.551**	.152	-.264	1
	Sig. (2-tailed)	.000	.371	.114	
	No.	37	37	37	37

**. Correlation is significant at the 0.01 level (2-tailed).

Table 16 Nonlinear ITS modeling

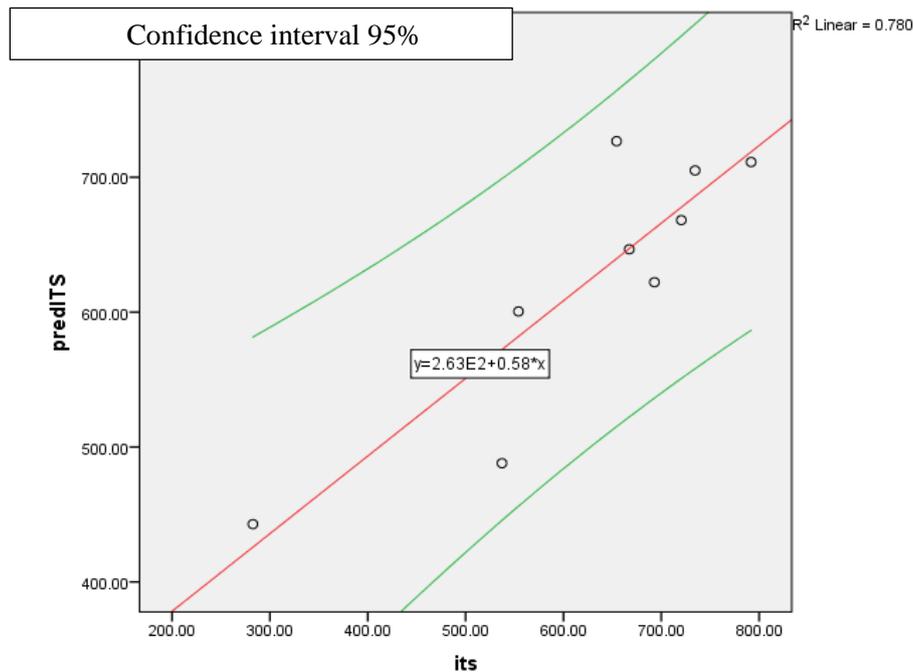
Developed model	$ITS = c1 + c2 * sbs - c3 * sbs^2 + c4 * sbs^3 + c5 * bc - c6 * bc^2 - c7 * ft$			
Parameter Estim.				
Parameter	Estim.	Std. Err.	95% Confidence Interval	
			Lower Bound.	Upper Bound.
c1	-7647.534	1145.557	-9987.073	-5307.994
c2	34.169	9.829	14.096	54.242
c3	1.092	.317	.445	1.740
c4	.011	.003	.005	.017
c5	2607.087	370.707	1850.003	3364.170
c6	209.286	29.821	148.383	270.189
c7	4.226	3.959	-3.860	12.312

Table 17 ANOVA for ITS modeling

ANOVA ^a			
Source	Sum of Squares	df	Mean Squares
Regression	16602904.820	7	2371843.545
Residual	93367.856	30	3112.262
Uncorrected Total	16696272.670	37	
Corrected Total	518335.159	36	

Dep. variable: ITS

a. R squared = 1 - (Residual Sum of Squares) / (Corrected Sum of Squares) = .820.

**Figure 4 comparisons between the experimental and predicted values of ITS.****5. Conclusion.**

From the statistical analysis of this research study, the following can be concluded:

1. General well-known linear and nonlinear model offered by available software could not represent the resulted values of mechanical, volumetric and durability properties in acceptable models.
2. Modeling the OGFC volumetric, mechanical, and durability characteristics with reference to mix design inputs is achievable and satisfactory in terms of prediction and the significant of input parameters with more complicated multi-variable non-linear models.
3. Permeability model is proven to be predictive from filler type, polymer content, and binder content. At the same time and within models' boundaries, the filler type has the most significant correlation to permeability, then binder content and lastly polymer content.
4. Moisture sensitivity model is proven to be predictive from filler type, polymer content, and binder content. At the same time and within models' boundaries, filler type has the most significant correlation to TSR, then polymer content and lastly binder content.
5. ITS model is proven to be predictive from filler type, polymer content, and binder content. Simultaneously and within models' boundaries, polymer content has the most significant correlation to ITS, then filler type and lastly binder content.

CONFLICT OF INTERESTS.

- There are no conflicts of interest.

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خصائص النماذج الاحصائية للخلطات النفاذة الاحتكاكية

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الخلاصة:

الطبقات النفاذة الاحتكاكية هي نوع خاص من الخلطات التي تستعمل كطبقة نهائية فوق سطح الخلطات الاعتيادية حيث ازداد استخدامها حول العالم وذلك لخواصها العديدة مثل الاحتكاك، السلامة، والفوائد البيئية، الخ. تضمن هذا البحث بعض الخواص المختبرية المختارة للخلطات النفاذة تم اختيارها للتحليل الاحصائي والتي تعتمد على مدخلات تصميم الخلطة. قوة الشد الغير مباشرة (ITS)، وحساسية الماء (TSR)، والنفاذية (K) اختيرت للخواص الميكانيكية، والديمومة، والحجمية، على التوالي، وهذه الخواص تمثل المتغيرات التابعة لكل موديل احصائي. حيث ان نوع المادة المالئة كغبار الركام الاعتيادي والسمنت البورتلاندي الاعتيادي (CMF, OPC)، نسبة الاسفلت (BC)، ونسبة البوليمر المضاف (SBS) تمثل المتغيرات المستقلة لكل الموديلات الاحصائية. الموديلات الاحصائية المتولدة توفر اداة تنبأ قابلة للتحقق حيث كانت قيم R^2 هي 0.781، 0.821، 0.820، على التوالي للموديلات الاحصائية المتولدة، كما أنها ساعدت على قياس أهمية كل متغير مستقل. على سبيل المثال، نوع المادة المالئة يؤثر بشكل كبير على خصائص حساسية الماء، حيث كان مقدار ارتباط (0.752). من خلال هذه الدراسة نكتشف أن التحليل الاحصائي هي اداة تنبأ قابلة للتحقق لوصف خصائص وأداء الخلطات النفاذة الاحتكاكية من حيث الخصائص الحجمية والميكانيكية والمتانة.

الكلمات الدالة: خرسانة اسفلتية، الطبقات النفاذة، الاسفلت المعدل مع البوليمر، التحليل الاحصائي.