



A Review of Preparation and Characterization of Additively Manufactured Stainless Steel

Rania Ali¹, Basem Al-Zubaidy²

^{1,2}Department of Metallurgical Engineering, College of Materials Engineering,
University of Babylon, Babylon, Iraq

raniaalobaidy96@gmail.com

Received:	25/6/2023	Accepted:	31/7/2023	Published:	20/9/2023
-----------	-----------	-----------	-----------	------------	-----------

Abstract

In today's world, ADDITIVE MANUFACTURING (AM) is a well-known method for creating true three-dimensional objects, either out of metals, ceramics, plastics, or a combination of these materials. ADDITIVE MANUFACTURING (AM) is connected with a series of rapid heating and cooling cycles, as well as substantial temperature gradients, which result in the development of complicated thermal histories, which have a direct impact on the resulting microstructures. Due to the nature of this dynamic and far-from-equilibrium process, different microstructural features emerge. For instance, these are likely to induce changes in the corrosion characteristics of ADDITIVE MANUFACTURING (AM) stainless steels, which have superior mechanical properties and corrosion resistance when manufactured using other production methods. Because such modifications are not fully understood at this time, inconsistencies and conflicts in the literature on the corrosion behaviour of ADDITIVE MANUFACTURING (AM) stainless steels are regularly seen. The preparation and characterization of additively made stainless steel is the subject of this work, which provides a critical assessment. In terms of producing huge metallic structures at high deposition rates and cheap costs, WIRE ARC ADDITIVE MANUFACTURING (WAAM) has emerged as a viable method. This article reviews some ADDITIVE MANUFACTURING (AM) methods used mostly with metallic materials focusing on the WIRE ARC ADDITIVE MANUFACTURING (WAAM) of stainless steel.

Keywords: ADDITIVE MANUFACTURING (AM), additive manufacturing of Metals, WIRE ARC ADDITIVE MANUFACTURING (WAAM) of Stainless steel.

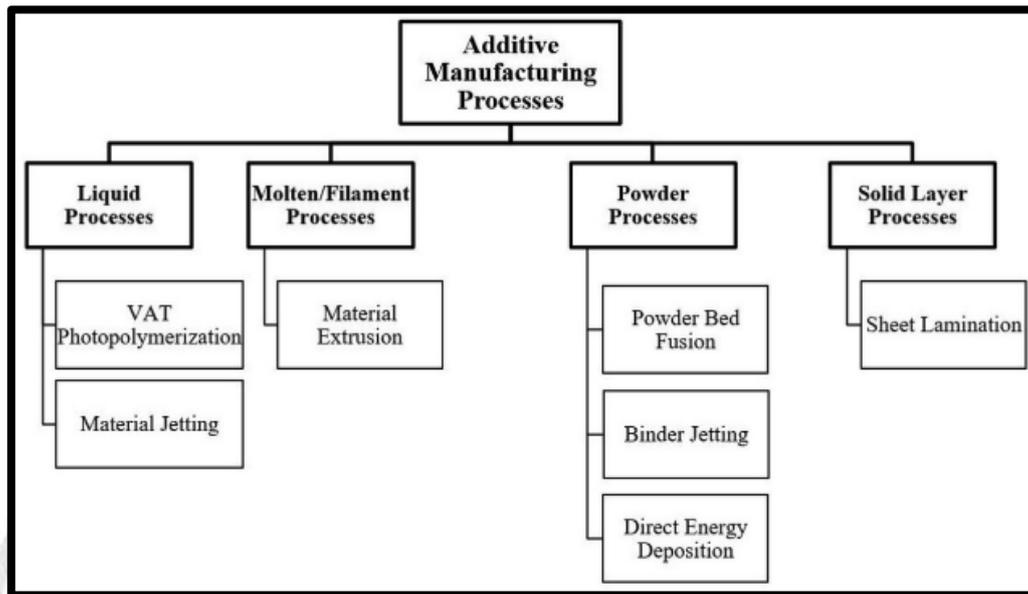


Figure (1): Classification of ADDITIVE MANUFACTURING (AM) processes depending on adhesion and bonding techniques [1]

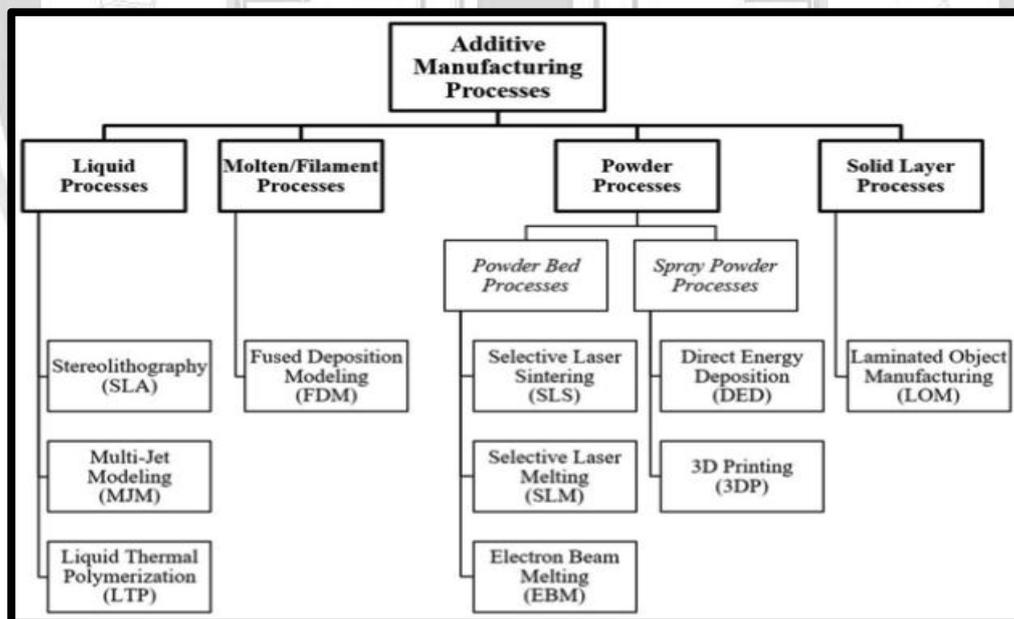


Figure (2) Processes for additive manufacturing [7].

2.1 Powder Bed Processes

2.1.1 Selective Laser Sintering.

SELECTIVE LASER SINTERING (SLS) is a layer-by-layer additive manufacturing technology that uses fine powder to produce a product. An even layer of powder is applied using a coater arm to create a level, Figure 3a depicts a construction site with a smooth, uniform surface. A laser beam is focused towards the powder layer to do a cross-sectional scan of the part. It is necessary



to repeat the printing process until all of the layers have been produced [11, 12]. Particle binding processes include solid-state sintering, chemically induced binding, liquid-phase sintering, and partial melting. During solid-state sintering, the warmed powder melts between the melting point and half of the melting point. Binder components are absent from chemically induced binding, while metal atoms combine with oxygen to form a binding substance that helps to fuse the powder. It's possible to use the same material as both the structural material and the binder in liquid-phase sintering or partial melting [14]. SELECTIVE LASER SINTERING (SLS) can treat a wide variety of materials, allowing it to be used in a wide range of industries.

2.1.2 Selective Laser Melting.

It is the goal of full melting of powders to generate dense, mechanically similar objects. To achieve the same purpose, SELECTIVE LASER MELTING (SLM) technology was developed. All metals have the potential to be candidates, however, processing alters the behavior of certain. Differences in laser absorption reactions, surface tensions, and viscosities are examples of these kinds of variations. SELECTIVE LASER MELTING (SLM) metals are restricted by these issues [13]. Single-material powders and alloyed powders are the two basic types of SELECTIVE LASER MELTING (SLM) powders. Powders made from only one type of material, such as titanium, are known as single-material powders. Even though tests show a near-total density of 100%, excessive thermal loads can lead to fissures. Ti-6Al-4V and steel powders are two common alloyed materials used in alloyed powder formative processes. Due to their lack of ductility, these materials' mechanical characteristics are nearly identical to bulk materials [15]. Non-ferrous metals, such as titanium, aluminum, and copper, can be processed using SELECTIVE LASER MELTING (SLM) as shown Figure 3b. Due to increased energy consumption, melt pool instability and part shrinkage are becoming issues [16].

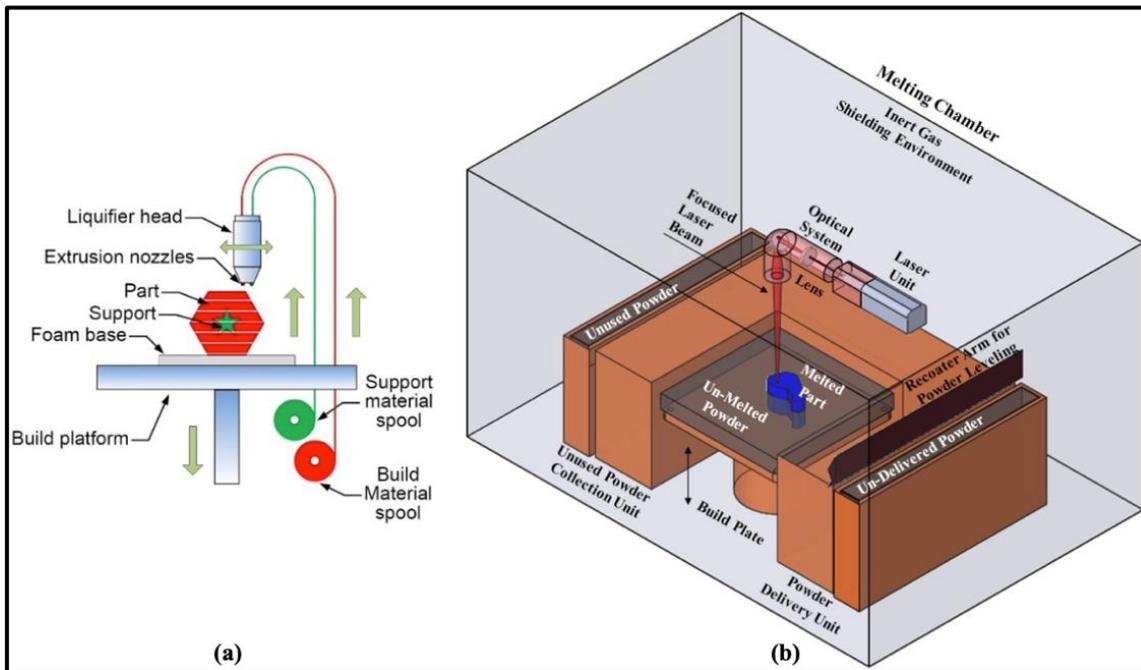


Figure. 3: (a) Fused deposition modelling [9, 10], and (b) selective laser sintering [11, 12] processes.

2.1.3 Electron Beam Melting

Because an electron gun melts warmed powder instead of a laser source for melting powder, ELECTRON BEAM MELTING (EBM) has more power because its build rate is faster than that of SELECTIVE LASER MELTING (SLM). In the case of metallic applications, powder bed techniques are a popular choice. In metal fabrication, ELECTRON BEAM MELTING (EBM) is now preferred, however, it is constrained by the material's electrical conductivity and the need to operate in a vacuum. SELECTIVE LASER MELTING (SLM), on the other hand, is more adaptable due to these drawbacks [17].

2.2 Spray Powder Processes

2.2.1 Direct Energy Deposition.

3D Cladding and Welding are two methods of DIRECT ENERGY DEPOSITION (DED) , which is an ADDITIVE MANUFACTURING (AM) process. When a laser or plasma beam melts the metal powder, it forms layers in the 3D Cladding process (see Figure. 4 [18]). Laser Metal Deposition, Laser Engineered Net Shaping, and Laser Consolidation are all laser-based processes. A nozzle feeds metal powder to the substrate, which is then laser melted to create Laser Metal Deposition (LMD) or LC. An extremely versatile technology, it can restore metal pieces that cannot be mended using other methods. These materials, which include nickel-based superalloys, cobalt



alloys, titanium alloys, and steel [19], have the potential to be used to coat, manufacture, and rebuild complicated components. An inert gas atmosphere of argon or helium or nitrogen is used to keep the oxidation of the powder to a minimum during the plasma-based process known as Plasma Deposition Manufacturing (PDM). Plasma beams can't remove all oxygen from commercially available gas; hence, some oxidized particles can still form while the powder melts and solidifies. For low-volume metals, Plasma Deposition Manufacturing (PDM) is a viable 3D part generation method [20]. It is a wire-based method called Shaped Metal Deposition (SMD) [21] that uses small-diameter wire to melt and bond to the preceding layers. When compared to laser deposition or electron beam welding, Shaped Metal Deposition (SMD) has the advantage of being able to use a greater variety of metals. Wire has a smaller surface area than powder, therefore oxidized particles have fewer chances to develop. Despite its promise, there are numerous issues identified in the literature, mostly linked to the regulation of the weld pool and its impact on dimensional and geometrical accuracies. In addition, this technology is capable of producing extremely dense and massive pieces with mechanical qualities comparable to cast metal [21].

2.3 Inkjet 3D Printing.

There are two primary types of inkjet 3D printing: binder jetting and material jetting. Using an inkjet head to selectively spray and print a binder liquid onto a powder bed, the binder jetting three-dimensional printing (3DP) binds the powder particles one layer at a time. Post-processing is necessary to ensure that the produced parts have suitable mechanical strength. A more common method of layering a model is through the inkjet head with droplets of the building material in a liquid state. After the droplets are sprayed, an Ultraviolet laser (UV) laser is passed through each layer to cure them [22]. Binder selection can have a considerable impact on a part's mechanical strength and characteristics, making it a difficult component of three-dimensional printing (3DP). A variety of biomedical applications use the three-dimensional printing (3DP) method because of its ability to create unique biocompatible devices. This includes clinical investigations as well as surgical trainers, custom reconstructive and orthopaedic implants, tissue engineering, and dental repairs. The quality of the finished surface is another issue that arises in three-dimensional printing (3DP) techniques. As a result, one of the primary research concerns for this technique is increasing the surface finish through intelligent powder distribution or the use of small particle sizes [23].

shapes and a bonding tool to heat and press together the solid layers. A high-speed ADDITIVE MANUFACTURING (AM) technique as shown Table 1, Laminated Object Manufacturing (LOM) is five to ten times quicker than conventional processes, although it has significant difficulties in obtaining geometric accuracy, surface smoothness, and desirable material qualities. [25].

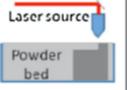
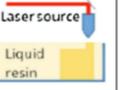
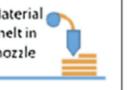
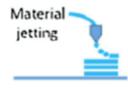
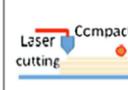
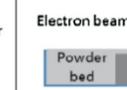
Additive Manufacturing (AM) Processes														
Process	Laser Based AM Processes				Extrusion Thermal	Material Jetting	Material Adhesion	Electron Beam						
	Laser Melting		Laser Polymerization											
Process Schematic														
Name Material	SLS		DMD		SLA		FDM		3DP		LOM		EBM	
	SLM		LENS		SGC		Robocasting		IJP		SFP			
	DMLS		SLC		LTP				MJM					
			LPD		BIS				BPM					
					HIS				Thermojet					
Bulk Material Type	Powder		Liquid		Solid									

Table 1 Additive Manufacturing Processes technologies [26].

2.6 Wire Arc Additive Manufacturing

Because of the great manufacturing efficiency and low forming costs of the wire arc additive manufacturing method (WIRE ARC ADDITIVE MANUFACTURING (WAAM)), it is capable of producing completely dense and large-dimensional items with lower manufacturing costs than powder-based ADDITIVE MANUFACTURING (AM) processes [29]. Compared to metal powder, the primary cost of metal wire is around 10% higher [28]. With the addition of WIRE ARC ADDITIVE MANUFACTURING (WAAM) machines, arc welding robots may be quickly converted into WIRE ARC ADDITIVE MANUFACTURING (WAAM) machines, which are often less expensive than L-PBF and laser-DIRECT ENERGY DEPOSITION (DED) machines, respectively. Wires are heated to melting temperature before being melted and transported to the melt pool, where they solidify layer by layer, as depicted in Figure 5 [30]. WIRE ARC ADDITIVE MANUFACTURING (WAAM) is a direct energy deposition (DIRECT ENERGY DEPOSITION (DED)) welding technique adapted from classic arc welding technology [27]. WIRE ARC ADDITIVE MANUFACTURING (WAAM) sometimes referred to as shape welding in Europe and structural weld build-up in the United States, has been around for a while [31]. [32] As early as 1926, Baker [23] was granted his patent for using electric arcs as heat sources to create large things by spraying liquid metal into previously formed layers. Shape welding was used by Kussmaul in 1983 to produce 79 tons of high-strength 20MnMoNi5 steel in considerable quantities [31]. Late in the

twentieth century, the Germans employed WIRE ARC ADDITIVE MANUFACTURING (WAAM) (shape welding) to make main nuclear components [31].

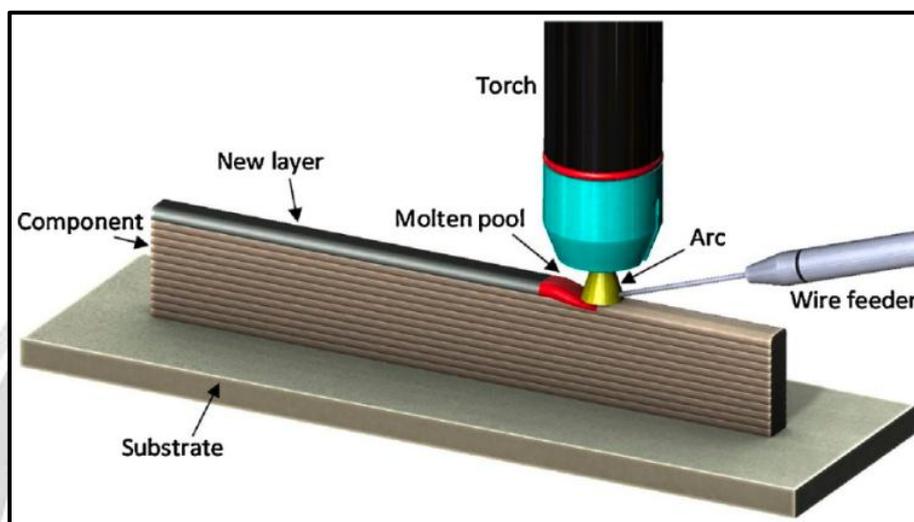


Figure 5. Diagrammatic sketch of the WIRE ARC ADDITIVE MANUFACTURING (WAAM) process [30].

3. Review of WIRE ARC ADDITIVE MANUFACTURING (WAAM) of Stainless-Steel

Feng et al, [34] use of plasma arc additive manufacturing to create Cr-Ni stainless steel components have been proposed in this research as a new and highly efficient approach to DOUBLE-WIRE FEED AND PLASMA ARC ADDITIVE MANUFACTURING (DWF-PAM)). DOUBLE-WIRE FEED AND PLASMA ARC ADDITIVE MANUFACTURING (DWF-PAM) processing's better bead appearance, microstructure, and mechanical properties were examined in the test components as a whole. In comparison to the single-wire feed and plasma additive manufacturing SINGLE-WIRE FEED AND PLASMA ADDITIVE MANUFACTURING (SWF-PAM) technique, the results demonstrate that the deposition rate in the DOUBLE-WIRE FEED AND PLASMA ARC ADDITIVE MANUFACTURING (DWF-PAM) process rose by an average of 1.06 times at the same procedure settings. The DOUBLE-WIRE FEED AND PLASMA ARC ADDITIVE MANUFACTURING (DWF-PAM)-processed sample had a considerable number of completely grown equiaxed ferrite (CGEF) grains near the following layer's interface, while the SINGLE-WIRE FEED AND PLASMA ADDITIVE MANUFACTURING (SWF-PAM)-processed sample had an equal amount of incompletely grown equiaxed ferrite grains in the same location. The DOUBLE-WIRE FEED AND PLASMA ARC ADDITIVE MANUFACTURING (DWF-PAM)-processed materials' ultimate tensile strengths and elongation rates were significantly enhanced by the CGEF grains. The maximum increase in elongation rate was 176 per cent, and the average increase in final



tensile strength was 10.2%. A fine-grained microstructure and higher mechanical characteristics may be achieved by using the DWF process instead of the SWF process to manufacture components. In addition, with the DOUBLE-WIRE FEED AND PLASMA ARC ADDITIVE MANUFACTURING (DWF-PAM) technique, a greater deposition rate is possible shown in table 2.

Ahsan et al, [37] used BAMSs (bimetallic additively produced structures) to reduce post-processing-induced regional mechanical degradation by replacing traditionally constructed functionally graded components. These structures are constructed using fusion welding methods. Using a wire + arc additive manufacturing (WIRE ARC ADDITIVE MANUFACTURING (WAAM)) approach based on gas metal arc welding(GMAW). This work fabricates a BAMS by layering austenitic stainless steel and Inconel 625. They found that it was there was no recognition of the interface between the layers of the two materials. This results in a seamless compositional transition. An electron backscattered diffraction (EBSD) examination of the interface shows that both materials are austenite with an FCC crystallographic structure, with long-elongated grains in the 001> direction exhibiting a smooth and cross-interface crystallographic growth. At the interface, neither material differed significantly in hardness from the other, with values ranging from 220 to 240 HV for each. Stainless steel failed at a tensile strength and elongation of 600 MPa and 40%, respectively. According to the findings of this study, WIRE ARC ADDITIVE MANUFACTURING (WAAM) can make BAMS that have higher properties shown in table 2.

Wu et al, [33] used 316L stainless steel welding wire to create 30-layered thin-walled samples with a 2 mm thickness and up to 65mm height by using speed cold welding. It is found that the stability of the deposition process, macro morphology, structure, and mechanical qualities are affected by three process parameters (bottom current mode, scanning speed, and cooling time). Compared to other samples, sample #GRBC-30 cm/min-10 s had narrower third- and tenth-layer probability density curves, indicating a more stable process. While the three process parameters have some bearing on performance, their primary impact is on the morphology of the layer deposition. The deposition direction has a major impact on the hardness and tensile strength of the finished product. The bottom moulding and performance, as well as the deposition efficiency and process stability, are improved and stabilized through gradual, layer-by-layer current decrease. End formation is destabilized by increasing the scanning speed or reducing the cooling time, which lowers the effective deposition rate. All samples deposited are anisotropic, yet meet the requirements of the industry. All in all, the deposition in speed cold welding mode, with a cooling time of just 10 seconds, a scanning speed of 30 cm/min, and a rapidly decreasing bottom current demonstrates excellent stability shown in table 2.



Hosseini et al [35], wire-arc additive manufacture of duplex stainless steel blocks to study how microstructures change during heat cycles. High and low heat input–high interlayer temperatures (LHLT and HHLT) arc energies were used to create samples. For high heat input–high interlayer temperature (HHLT), interlayer temperatures of 150°C and 250°C were employed (HHHT). Various thermocouples were employed for recording heat cycles on the substrate and constructed layers. An in-depth examination of the microstructure was performed using O&SEM. LHLT and HHHT were able to create equivalent geometries with 14 and 15 layers of beads in each layer, respectively. At higher temperatures (over 600 °C), LHLT had more warming cycles than HHHT, although each layer was warmed for less time. The austenite content was 8 per cent higher in as-deposited LHLT beads that were cooled at a faster pace between 1200 and 800 °C. There were equal austenite fractions in both LHLT and HHHT samples throughout a wide range of additively created samples that had been heated several times. The HHHT sample had a larger percentage of secondary phases as a result of the prolonged reheating at a high temperature. There was an adequate austenite fraction (35–60 per cent) with just a modest number of secondary phases in the majority of wire-arc additively manufactured duplex stainless steel samples (800–1200 degrees Celsius) shown in table 2.

Rumman and Ali [36] used the wire with arc additive manufacturing (WIRE ARC ADDITIVE MANUFACTURING (WAAM)) method based on gas metal arc welding (GMAW) to create metal products in nearly net shape products. WIRE ARC ADDITIVE MANUFACTURING (WAAM) is flexible enough to create a single component from multiple materials sequentially or simultaneously. A key concern is design. This work generated components by sequentially fusing low-carbon steel and AISI 316L stainless steel (SS). To do this a new M2WIRE ARC ADDITIVE MANUFACTURING (WAAM) system was built utilizing commercial resources. The system's use for WIRE ARC ADDITIVE MANUFACTURING (WAAM) and M2WIRE ARC ADDITIVE MANUFACTURING (WAAM) has been proved using two metals – LOW-CARBON STEEL (LCS) and stainless steel (SS)– and two designs. The mechanical, microstructural, and composition of the various specimens were compared to a single LOW-CARBON STEEL (LCS) and stainless steel (SS) material specimen. No welding defects were found at the joint between the two components. However, the interface hardness increased considerably. The EDS analysis attributes the increase in hardness to chromium diffusion from the stainless steel (SS) side into the LOW-CARBON STEEL (LCS) side. Despite the interface's varying hardness, the failure occurred on the LOW-CARBON STEEL (LCS) side, away from the contact. The UTS and elongation of the multi-material specimen are essentially identical. LOW-CARBON STEEL (LCS), being the weaker of the two materials used, failed. The WIRE ARC ADDITIVE MANUFACTURING (WAAM) technique can properly combine LOW-CARBON STEEL (LCS) and SS, according to this study's findings. Although WIRE ARC ADDITIVE MANUFACTURING (WAAM) has welding strength equivalent to steel, it is



found to be less ductile. Heat treatment of Wire arc additive manufacturing (WAAM) ed parts may improve yield strength and ductility, however, this has not been evaluated as shown in table 2.

Table 2 Process parameters affecting the macro morphology of WIRE ARC ADDITIVE MANUFACTURING (WAAM) stainless steel parts

WIRE ARC ADDITIVE MANUFACTURING (WAAM) Techniques	Material	Process Parameters	Macroscopic Characteristics	References
MIG	316L (austenitic) stainless steel	Welding current mode Increasing scanning speed Gradual reduction of bottom current	Improves bottom formation The unevenness of both ends	[34]
PAM PAM: SINGLE-WIRE FEED AND PLASMA ADDITIVE MANUFACTURING (SWF-PAM), THE DOUBLE-WIRE FEED AND PLASMA ARC ADDITIVE MANUFACTURING (DWF-PAM)	H00Cr21Ni10 (austenitic) stainless steel	SINGLE-WIRE FEED AND PLASMA ADDITIVE MANUFACTURING (SWF-PAM): single-wire feed and plasma additive manufacturing THE DOUBLE-WIRE FEED AND PLASMA ARC ADDITIVE	Slightly better surface quality than that of Double-wire feed and plasma additive manufacturing ////	[35]



		<p>MANUFACTURING (DWF-PAM):</p> <p>double-wire feed and plasma additive manufacturing</p> <p>Increasing scanning speed</p>	Better surface quality	
GMAW	Type-2209 (duplex) stainless steel	<p>Deposition path</p> <p>Alternating direction deposition path</p> <p>One-direction deposition path</p>	<p>Uniform layer height</p> <p>Uneven sides: the start side was higher than the end side.</p>	[36]
GMAW	H08Mn2Si low-carbon steel	<p>Decreasing interlay temperature</p> <p>Increasing scanning speed</p> <p>Increasing wire feeding speed</p>	<p>Surface roughness decreases</p> <p>Surface roughness increases</p> <p>Surface</p>	[37]



wire is melted and transported to the melt pool during the WIRE ARC ADDITIVE MANUFACTURING (WAAM) process. Indirect energy deposition (DIRECT ENERGY DEPOSITION (DED)) is a method that was developed from traditional arc welding technology [7].

WIRE ARC ADDITIVE MANUFACTURING (WAAM) , also known as shape welding in Europe and structural weld build-up in America, has been around for quite some time [20]. Baker [20] received a patent in early 1926 for "the use of an electric arc as a heat source to manufacture bulk objects by spraying molten metal into the formed layers," which described "the use of an electric arc as a heat source to manufacture bulk objects by spraying molten metal into the formed layers" A 79-ton piece of high-strength 20MnMoNi5 steel was produced by Kussmaul in 1983 [20] using shape welding on an industrial scale. Germany used WIRE ARC ADDITIVE MANUFACTURING (WAAM) (shape welding) to construct the bulk of its nuclear weapons in the late twentieth century [12]. In the aerospace industry (stretched panels, wing ribs), nuclear energy, maritime (ship propeller), and architectural (steel bridge) [14], WIRE ARC ADDITIVE MANUFACTURING (WAAM) has already been successfully implemented.

5. Concluding Remarks

ADDITIVE MANUFACTURING (AM) stainless steels frequently have a multidimensional and non-homogeneous microstructure, as well as high residual stress, which complicates corrosion behaviour and processes. While there is considerable diversity in the corrosion parameters of ADDITIVE MANUFACTURING (AM) stainless steels documented in the literature, based on the current state of the art, some basic conclusions can be formed.

Porosity affects the corrosion parameters of ADDITIVE MANUFACTURING (AM) stainless steel such as passivity, pitting, and erosion-corrosion in a negative way. Due to the presence of porosity, low-density ADDITIVE MANUFACTURING (AM) stainless steels have lower pitting corrosion resistance. Because the necessary conditions for pit stability may be easily produced in the presence of LOF pores, such pores, in particular LOF pores, were identified as more sensitive sites to pitting corrosion. The role of pores in pit initiation in ADDITIVE MANUFACTURING (AM) stainless steels, on the other hand, is still being researched and debated.

Due to the absence of detrimental inclusions/precipitates, such as MnS inclusions, the pitting corrosion resistance of high-density ADDITIVE MANUFACTURING (AM) stainless steels is generally higher than that of their conventionally manufactured counterparts. However, using post-ADDITIVE MANUFACTURING (AM) heat treatment to release residual stress in ADDITIVE MANUFACTURING (AM) stainless steels, especially over 1000°C, may result in the formation of detrimental inclusions/precipitates, resulting in lower pitting corrosion resistance.



ADDITIVE MANUFACTURING (AM) stainless steels have unique microstructural characteristics that cause a variety of surprising localized corrosion behaviours. ADDITIVE MANUFACTURING (AM) stainless steels have a lower capacity to passivate, which leads to a worse erosion-corrosion resistance. ADDITIVE MANUFACTURING (AM) austenitic stainless steels show significantly better resistance to IGC when subjected to long-term sensitisation heat treatment, which has been attributed to a high density of twins and low-angle grain boundaries in ADDITIVE MANUFACTURING (AM) materials.

Corrosion research on ADDITIVE MANUFACTURING (AM) stainless steels is still in its early phases, and additional work is needed to quantify the resistance of ADDITIVE MANUFACTURING (AM) stainless steels to key kinds of localised corrosion such as crevice corrosion and galvanic corrosion under various and practical corrosion environments.

References

- [1] ASTM, "Standard Terminology for Additive Manufacturing - General Principles - Terminology," in ISO/AMERICAN SOCIETY FOR TESTING AND MATERIALS (ASTM) 52900, ed. West Conshohocken, PA, 2015.
- [2] H. A. Youssef, H. A. El-Hofy, and M. H. Ahmed, Manufacturing Technology: Materials, Processes, and Equipment. International Edition: Taylor & Francis Group, CRC Press, 2012.
- [3] N. Guo and M. C. Leu, "Additive Manufacturing: Technology, Applications and Research Needs," Frontiers of Mechanical Engineering, vol. 8, pp. 215-243, 2013.
- [4] I. Gibson, D. Rosen, and B. Stucker, Additive Manufacturing Technologies; 3D Printing, Rapid Prototyping, and Direct Digital Manufacturing. New York, USA: Springer, 2015.
- [5] K. V. Wong and A. Hernandez, "A Review of Additive Manufacturing," International Scholarly Research Network (ISR) Mechanical Engineering, vol. 2012, 2012.
- [6] C. W. Hull, "Apparatus for Production of Three-Dimensional Objects by Stereolithography," United States Patent, 1986.
- [7] Yusuf, S.M.; Cutler, S.; Gao, N. Review: The Impact of Metal Additive Manufacturing on the Aerospace Industry. Metals 2019, 9, 1286.
- [8] H. A. El-Hofy, Advanced Machining Processes; Nontraditional and Hybrid Machining Processes. International Edition: McGraw-Hill, 2005.
- [9] F. Ning, W. Cong, J. Qiu, J. Wei, and S. Wang, "Additive manufacturing of carbon fiber reinforced thermoplastic composites using fused deposition modeling," Composites Part B: Engineering, vol. 80, pp. 369-378, 2015.
- [10] M. Yakout and M. A. Elbestawi, "Additive Manufacturing of Composite Materials: An Overview," in The 6th International Conference on Virtual Machining Process Technology, Montréal, Canada, 2017.



- [11] J. Mireles, D. Espalin, D. Roberson, B. Zinniel, F. Medina, and R. Wicker, "Fused Deposition Modeling of Metals," in International Solid Freeform Fabrication Symposium, USA, 2012, pp. 836-845.
- [12] M. Yakout, M. A. Elbestawi, and S. C. Veldhuis, "On the characterization of stainless steel 316L parts produced by selective laser melting," International Journal of Advanced Manufacturing Technology, vol. Online First, pp. 1-22, 2017.
- [13] J.-P. Kruth, P. Mercelis, L. Froyen, and M. Rombouts, "Binding Mechanisms in Selective Laser Sintering and Selective Laser Melting," in International Solid Freeform Fabrication Symposium, USA, 2004.
- [14] J.-P. Kruth, M. C. Leu, and T. Nakagawa, "Progress in Additive Manufacturing and Rapid Prototyping," CIRP Annals - Manufacturing Technology, vol. 47, pp. 525-540, 1998.
- [15] C. Over, W. Meiners, K. Wissenbach, M. Lindemann, and G. Hammann, "Selective Laser Melting: A New Approach for the Direct Manufacturing of Metal Parts and Tools," in International Conference on Laser Assisted Net Shape Engineering, Furth, Germany, 2001.
- [16] D. D. Gu, W. Meiners, K. Wissenbach, and R. Poprawe, "Laser additive manufacturing of metallic components: materials, processes and mechanisms," International Materials Reviews, vol. 57, pp. 133-164, 2012/05/01 2012.
- [17] K. M. Taminger and R. A. Hafley. (2006) Electron Beam Freeform Fabrication for Cost Effective Near-Net Shape Manufacturing. Cost-Effective Manufacture via Net-Shape Processing (RTO-MP-AVT-139). 16 (1-10).
- [18] R. J. Urbanic, S. M. Saqib, and K. Aggarwal, "Using Predictive Modeling and Classification Methods for Single and Overlapping Bead Laser Cladding to Understand Bead Geometry to Process Parameter Relationships," Journal of Manufacturing Science and Engineering, vol. 138, pp. 051012 (1-13), 2016.
- [19] L. Xue and M. Ul-Islam, "Laser Consolidation – A Novel One-Step Manufacturing Process for Making Net-Shape Functional Components," in Cost Effective Manufacture via Net-Shape Processing (RTO-MP-AVT-139), France, 2006, pp. (15) 1-14.
- [20] H. Zhang, J. Xu, and G. Wang, "Fundamental Study on Plasma Deposition Manufacturing," in International Conference on Open Magnetic Systems for Plasma Confinement, Jeju Island, Korea, 2003.
- [21] B. Baufeld, O. V. d. Biest, and R. Gault, "Additive Manufacturing of Ti-6Al-4V Components by Shaped Metal Deposition: Microstructure and Mechanical Properties," Materials & Design, vol. 31, pp. S106-S111, 2010.
- [22] W. Gao, Y. Zhang, D. Ramanujan, K. Ramani, Y. Chen, C. B. Williams, et al., "The Status, Challenges, and Future of Additive Manufacturing in Engineering," Computer-Aided Design, 2015.
- [23] M. Lanzetta and E. Sachs, "Improved Surface Finish in 3D Printing Using Bimodal Powder Distribution," Rapid Prototyping Journal, vol. 9, pp. 157-166, 2003.
- [24] M. Feygin, A. Shkolnik, M. N. Diamond, and E. Dvorsky, "Laminated Object Manufacturing System " USA Patent US5730817A, 1996.
- [25] E. C. Santos, M. Shiomi, K. Osakada, and T. Laoui, "Rapid Manufacturing of Metal Components by Laser Forming," International Journal of Machine Tools & Manufacture vol. 46, pp. 1459-1468, 2006.



- [26] Bikas H, Stavropoulos P, Chryssolouris G. Additive manufacturing methods and modelling approaches: a critical review. *Int J Adv Manuf Technol* 2016;83:389–405.
- [27] Thapliyal, S. Challenges associated with the wire arc additive manufacturing (WIRE ARC ADDITIVE MANUFACTURING (WAAM)) of aluminum alloys. *Mater. Res. Express* 2019, 6, 112006.
- [28] Frazier, W.E. Metal Additive Manufacturing: A Review. *J. Mater. Eng. Perform.* 2014, 23, 1917–1928.
- [29] Syed, W.U.H.; Pinkerton, A.; Li, L. A comparative study of wire feeding and powder feeding in direct diode laser deposition for rapid prototyping. *Appl. Surf. Sci.* 2005, 247, 268–276.
- [30] McAndrew, A.; Rosales, M.A.; Colegrove, P.; Hönnige, J.R.; Ho, A.; Fayolle, R.; Eytayo, K.; Stan, I.; Sukrongpang, P.; Crochemore, A.; et al. Interpass rolling of Ti-6Al-4V wire + arc additively manufactured features for microstructural refinement. *Additive Manufacturing* 2018, 21, 340–349.
- [31] Korzhyk, V.; Khaskin, V.; Voitenko, O.; Sydorets, V.; Dolianovskaia, O. Welding Technology in Additive Manufacturing Processes of 3D Objects. *Mater. Sci. Forum* 2017, 906, 121–130.
- [32] Wu, B.; Pan, Z.; Ding, D.; Cuiuri, D.; Li, H.; Xu, J.; Norrish, J. A review of the wire arc additive manufacturing of metals: Properties, defects and quality improvement. *J. Manuf. Process.* 2018, 35, 127–139.
- [33] Wu, W.; Xue, J.; Wang, L.; Zhang, Z.; Hu, Y.; Dong, C. Forming Process, Microstructure, and Mechanical Properties of Thin-Walled 316L Stainless Steel Using Speed-Cold-Welding Additive Manufacturing. *Metals* 2019, 9, 109.
- [34] Feng, Y.; Zhan, B.; He, J.; Wang, K. The double wire feed and plasma arc additive manufacturing process for deposition in Cr-Ni stainless steel. *J. Mater. Process. Technol.* 2018, 259, 206–215.
- [35] Hosseini, V.; Högstöm, M.; Hurtig, K.; Bermejo, M.A.V.; Stridh, L.-E.; Karlsson, L. Wire-arc additive manufacturing of a duplex stainless steel: Thermal cycle analysis and microstructure characterization. *Weld. World* 2019, 63, 975–987.
- [36] Md. Rumman Ul Ahsan and Ali Newaz Mohammad Tanvir & Taylor Ross & Ahmed Elsayy & Min-Suk Oh & Duck Bong Kim, " Fabrication of bimetallic additively manufactured structure (BAMS) of low carbon steel and 316L austenitic stainless steel with wire 1 arc additive manufacturing", 2019
- [37] Md. R.U. Ahsan, Xuesong Fan, Gi-Jeong Seo, Changwook Ji, Mark Noakes, Andrzej Nycz, Peter K. Liaw, Duck Bong Kim, " Microstructures and mechanical behavior of the bimetallic additively-manufactured structure (BAMS) of austenitic stainless steel and Inconel 625", 2020

مراجعة أدبية لتحضير وتوصيف الفولاذ المقاوم للصدأ المصنوع مضافاً

رانيا علي حمودي باسم محسن الزبيدي

قسم الهندسة المعدنية/ كلية هندسة المواد/جامعة بابل، بابل، العراق

الخلاصة

في عالم اليوم، يعد التصنيع بالإضافة طريقة معروفة لإنشاء نماذج ثلاثية الأبعاد، إما من المعادن أو السيراميك أو البلاستيك أو مزيج من هذه المواد. يرتبط التصنيع بالإضافة بسلسلة من دورات التسخين والتبريد السريعة، فضلاً عن التدرجات الكبيرة في درجات الحرارة، مما يؤدي إلى تطوير تواريخ حرارية معقدة، والتي لها تأثير مباشر على الهياكل الدقيقة للمواد الناتجة. نظراً لطبيعة هذه العملية الديناميكية والبعيدة عن التوازن، تظهر ميزات هيكلية مجهرية مختلفة. على سبيل المثال، من المحتمل أن تحدث تغييرات في خصائص التآكل للفولاذ المقاوم للصدأ المصنوع بتقنية الإضافة، والتي تتمتع بخصائص ميكانيكية فائقة ومقاومة للتآكل عند تصنيعها باستخدام طرق إنتاج أخرى. نظراً لأن مثل هذه التعديلات غير مفهومة تماماً في هذا الوقت، فإن التناقضات والاختلافات في الأدبيات المتعلقة بسلوك التآكل للفولاذ المقاوم للصدأ المصنوع مضافاً تظهر بانتظام. يعد تحضير وتوصيف الفولاذ المقاوم للصدأ المصنوع مضافاً موضوع هذا العمل، والذي يوفر تقييماً نقدياً. فيما يتعلق بإنتاج الهياكل المعدنية الضخمة بمعدلات ترسيب عالية وبتكلفة رخيصة، فقد برز التصنيع بالإضافة السلبي كطريقة قابلة للتطبيق. تستعرض هذه المقالة بعض طرق التصنيع بالإضافة المستخدمة في الغالب مع المواد المعدنية مع التركيز على التصنيع بالإضافة السلبي من الفولاذ المقاوم للصدأ.

الكلمات الدالة: التصنيع الإضافي (AM)، التصنيع الإضافي للمعادن، التصنيع الإضافي للقوس السلبي (WAAM) من الفولاذ المقاوم للصدأ.